

In-situ Characterization of the Thermal State of Resonant Optical Interferometers via Tracking of their Higher-order Mode Resonances

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Abstract

Thermal lensing in resonant optical interferometers such as those used for gravitational wave detection is a concern due to the negative impact on control signals and instrument sensitivity. In this paper we describe a method for monitoring the thermal state of such interferometers by probing the higher-order spatial mode resonances of the cavities within them. We demonstrate the use of this technique to measure changes in the Advanced LIGO input mode cleaner cavity geometry as a function of input power, and subsequently infer the optical absorption at the mirror surfaces at the level of 1 ppm per mirror. We also demonstrate the generation of a useful error signal for thermal state of the Advanced LIGO power recycling cavity by continuously tracking the first order spatial mode resonance frequency. Such an error signal could be used as an input to thermal compensation systems to maintain the interferometer cavity geometries in the presence of transients in circulating light power levels, thereby maintaining optimal sensitivity and maximizing the duty-cycle of the detectors.

1 Introduction

The second generation of kilometer-scale ground based laser interferometric gravitational wave detectors is currently under development, with aims of reaching unprecedented strain sensitivities and making the first direct detection of gravitational waves. Advanced LIGO (aLIGO) in the US consists of two 4km dual-recycled Fabry-Perot Michelson interferometers situated in Hanford, Washington and Livingston, Louisiana [1]. aLIGO incorporates many upgrades over the initial LIGO project[2], including improved seismic isolation and suspensions for the core optics, the addition of a signal recycling mirror, stable recycling cavities and an increase in the circulating light power. The increased circulating light power in particular places great importance on the ability to characterize the thermal state of the interferometer, because of the effects of thermal lensing associated with absorption in the core optics [3].

Optical cavities, such as those which make up the aLIGO interferometers, have a defined set of resonances which may be characterized by both their longitudinal spacing and transverse structure. For

any given longitudinal mode, an infinite set of transverse modes describes the spatial properties of the beam in a plane perpendicular to the propagation axis. In the case of an optical cavity with spherically curved mirrors, the higher-order transverse modes (HOMs) are well described by the Hermite-Gauss functions [4]. Measuring the eigenfrequencies of these HOMs provides a powerful method of characterizing an optical cavity.

Measurement of the spacing between the fundamental resonances has been used to measure the length of an optical resonator to a precision of ~ 5 ppm [5, 6]. Precise measurement of the width of the fundamental resonance, the so-called cavity pole, provides a measurement of the losses in a high finesse resonator with an accuracy of 2 ppm [7]. Measurement of the frequency spacing between the fundamental mode and the first excited modes can be used to measure the cavity Gouy phase to a level of $\sim 2 \cdot 10^{-2}$ [6] from which the radii of curvature of the mirrors can be inferred with additional information [5].

A number of other complementary techniques have been developed to characterize resonant interferometers. The dynamic response of optical cavities to laser frequency variations has been used to measure the length of the LIGO arms to a precision of $80 \mu\text{m}$ [8]. Their dynamic response to amplitude variations has been used to measure the round-trip loss at the 10 ppm level [9].

In this paper we report on the methods and results of two experiments which trace the thermal state of an optical cavity by monitoring the spacing between the fundamental mode and the first order spatial mode. In particular, this frequency spacing is used to infer the amount of total absorption in the aLIGO input mode cleaner (IMC) as well as to generate an error signal for thermal compensation of the aLIGO power recycling cavity (PRC), both of which are located at the LIGO Livingston Observatory (LLO).

The paper is organized as follows; Section 2 gives a general description of the technique used to measure the resonant frequencies of an optical cavity. Section 3 explains how one calculates the eigen-spectrum of an ideal resonator, and Section 4 shows how tracking of the first order resonance can be used to sense the thermal state of a resonator. Section 5 describes how this technique was applied to measure the absorption of the aLIGO IMC. Section 6 describes how the technique was used to generate an error signal of the thermal state of the aLIGO PRC. Finally, Section 7 closes with some conclusions and an outlook of how this technique might be applied in the future.

2 Measurement principle

In order to measure the eigenfrequencies of an optical cavity it is first necessary to control the resonance condition of the cavity for a fixed ‘carrier’ frequency. Control is typically accomplished with some variant of the Pound-Drever-Hall (PDH) technique [10, 11], whereby an error signal for the carrier frequency resonance condition is generated from the beat between fixed frequency RF phase modulation sidebands and the carrier light in reflection from the cavity. This error signal is applied as feedback to stabilize the relative fluctuations between the frequency of the laser and the length of the cavity.

An additional sideband (or pair of sidebands) with a tunable frequency offset to the carrier frequency may then be used to probe the eigenspectrum of the cavity. This can be accomplished by adding a pair of sidebands to the carrier beam with phase or amplitude modulation, or by injecting an auxiliary laser beam which is phase locked to the carrier beam. Using modulation has the advantage that the sideband fields are already aligned to the carrier beam, while using an auxiliary laser has the advantage of adding only a single sideband to the carrier beam, thus simplifying the analysis. Henceforth we do not consider the fixed frequency sidebands used for PDH control in this discussion; the term sidebands will be used only to describe the tunable frequency sidebands used for probing the cavity eigenspectra.

For the case of a tunable single sideband we may write the beam incident upon the cavity as

$$E_0 = E_c e^{-i\omega_0 t} \sum_{nm} b_{nm} U_{nm} + E_s e^{-i(\omega_0 + \Omega)t} \sum_{nm} c_{nm} U_{nm}, \quad (1)$$

where E_c and ω_0 are the field amplitude and frequency of the carrier, E_s is the field amplitude of the sideband, Ω is the offset frequency between the carrier and the sideband (the modulation frequency), U_{nm} are the functions describing the spatial structure of the HOMs of the cavity, and $|b_{nm}|^2$ ($|c_{nm}|^2$) quantifies how much carrier (sideband) power is in each of the HOMs.

When the offset frequency of the sideband is near a resonance for particular HOM, say the $n'm'$ mode, the beam transmitted through the cavity will be

$$E(t) = t(\omega_0)E_c e^{-i\omega_0 t} U_{00} + t(\omega_0 + \Omega)E_s e^{-i(\omega_0 + \Omega)t} c_{n'm'} U_{n'm'}, \quad (2)$$

where we have assumed for simplicity of exposition that the cavity is non-degenerate with a high finesse such that all non-resonant modes are completely reflected. Here $t(\omega_0)$ is the transmittance of the cavity to the 00 mode of the carrier which is assumed to be real, $t(\omega_0 + \Omega)$ is the transmittance of the cavity at frequency $\omega_0 + \Omega$ associated with which is near the resonance of the $n'm'$ mode.

Calculating the power in this beam gives

$$P = t(\omega_0)^2 E_c^2 |U_{00}|^2 + |t(\omega_0 + \Omega)|^2 E_s^2 c_{n'm'}^2 |U_{n'm'}|^2 + 2t(\omega_0)^2 E_c E_s c_{n'm'} \Re[U_{n'm'} U_{00}^* t(\omega_0 + \Omega)]. \quad (3)$$

Finally, integrating spatially over the incomplete cross section of the beam ∂ and extracting the terms which will show up after demodulation at the sideband offset frequency Ω gives

$$P_\Omega = 2t(\omega_0)^2 E_c E_s c_{n'm'} \int_{\partial} U_{n'm'} U_{00}^* \{ \Re[t(\omega_0 + \Omega)] \cos(\Omega t) + \Im[t(\omega_0 + \Omega)] \sin(\Omega t) \} dA, \quad (4)$$

where we have assumed that the Gaussian beam parameters are the same for the sideband and the carrier.

The transmittance coefficient for a two mirror spherical cavity is given by

$$t(\omega) = \frac{t_1 t_2 e^{-i \frac{L}{c} (\omega - \Omega_0)}}{1 - r_1 r_2 e^{-i 2 \frac{L}{c} (\omega - \Omega_0)}}, \quad (5)$$

where r_i and t_i are the reflectance and transmittance of the mirrors, L is the one way length of the cavity, and Ω_0 is the resonant frequency of the particular HOM. This function undergoes a rapid phase transition as Ω is swept through the resonance, allowing for a precise determination of the resonance frequency. More complicated and realistic optical resonators, including the aLIGO IMC have similar transmittance coefficients near a resonance.

From this result we can see that the two quadratures of the demodulated signal map out both quadratures of the complex transmittance coefficient of the optical cavity at each HOM resonance. The phase flip in the complex transmittance coefficient across the resonance of a given higher-order spatial mode gives an ideal signal for precisely determining the eigenfrequency of that mode.

The calculation can be generalized to show that the measurement principle still works with multiple sidebands, as in the case where a modulator is used rather than an auxiliary laser. In addition, a similar calculation shows that the measurement can also be made in reflection of an optical cavity with the only major difference being that the complex reflectance coefficient of the cavity is measured rather than the transmittance coefficient.

Notice that the signal in Eqn. (4) is proportional both to the amount of HOM power injected, captured in the coefficient $c_{n'm'}$, and the amount of HOM power detected, captured in the integral. The creation of higher-order modes in the sideband field is most easily achieved by partially occulting the input beam, thereby scattering the mostly Gaussian (HG₀₀) beam into a range of higher-order modes. This method has the advantage of creating many HOMs so that the various resonances of the optical cavity can be probed without any significant changes to the experimental setup.

It is also important that the measurement device is sensitive to the beat note between the carrier beam, which is in the HG₀₀ mode, and the components of the sideband beam which are in higher-order spatial modes HG _{nm} . Integrating over the full spatial profile of the beam by focusing it onto a photodiode would cause the experiment to be insensitive to this beat note, due to the orthogonality of the HG modes over an infinite transverse plane. The detection method employed in our experiments was to simply occult a portion of the beam before focusing it onto the photodetector, thus breaking the symmetry of the infinite transverse plane and providing sensitivity to a wide range of HOMs.

3 The eigenspectrum of an ideal resonator

Monochromatic radiation picks up an additional phase shift relative to a simple plane wave, known as the Gouy phase [12]. The amount of Gouy phase accumulated upon propagation is dependent on the spatial structure of the beam, but can be expressed rather simply when the beam is decomposed in the HG basis. In this basis, the Gouy phase accumulated by each HOM is related to that accumulated by the fundamental Gaussian ($n = m = 0$) mode simply by

$$\Psi_{nm} = (n + m + 1) \Psi_{00}, \quad (6)$$

where n and m specify the mode indices in the HG basis.

The geometry of a spherical optical cavity defines the modal basis of the beam that resonates within it. The accumulated round trip Gouy phase is therefore also defined by the cavity geometry. For a simple two mirror cavity the fundamental round-trip Gouy phase is given simply by

$$\Psi_{00} = 2 \cos^{-1}(\sqrt{g_1 g_2}) \quad (7)$$

where g_i are the standard cavity stability parameters given by

$$g_i = 1 - \frac{L}{R_i}, \quad (8)$$

where L is one half of the round-trip length of the cavity and R_i are the radii of curvature of the two mirrors.

The Gouy phase for a more complex cavity consisting of more than two mirrors is most easily calculated with ray matrix methods [12, 13]. The fundamental round-trip Gouy phase can be obtained from the expression [14, 15]

$$\Psi_{00} = 2 \cos^{-1} \left(\frac{B}{|B|} \sqrt{\frac{A + D + 2}{4}} \right), \quad (9)$$

where A , B , and D are three elements of the round-trip ABCD matrix.

The length of the cavity determines the frequency spacing between the longitudinal modes (successive resonances of any given transverse mode). This parameter, known as the free spectral range (FSR), is given for a cavity of round-trip length L by

$$f_0 = \frac{c}{L}. \quad (10)$$

In the experiments which follow the fundamental mode of the carrier will be held on resonance by a control system while the frequency of the sideband is shifted relative to this frequency. The frequency location of the resonances of the HOMs of an optical cavity are therefore given by

$$f_{nm} = \frac{c}{2\pi L} \text{mod}_{2\pi} [(n + m)\Psi_{00}] + l f_0, \quad (11)$$

for $l \in \mathcal{N}$. A cavity with an odd number of reflections per round trip splits the degeneracy between the modes with even and odd n by adding an extra π round trip phase for odd n modes. In this case the expression must be modified slightly to

$$f_{nm} = \frac{c}{2\pi L} \text{mod}_{2\pi} [(n + m)\Psi_{00} + \text{mod}_2(n)\pi] + l f_0. \quad (12)$$

4 The first order resonance as a thermal state sensor

Equation (11) shows that the eigenspectrum of a spherical optical cavity is fully determined by the round-trip Gouy phase and the length of the cavity. The round-trip Gouy phase is fully determined, in turn, by the cavity geometry as shown by Eqns. (7) and (8) or (9). Hence, a measurement of the location of any one of the higher-order resonances is a suitable probe for a change in the radius of curvature of one of the mirrors of a spherical optical cavity.

Winkler et. al. [16] derive an approximate relationship for the change in sagitta, δs , of an optic which is heated by optical absorption;

$$\delta s = \frac{\alpha}{4\pi\kappa} P_a, \quad (13)$$

where α is the coefficient of thermal expansion, κ is the thermal conductivity, and P_a is the absorbed power. The change in sagitta can be expressed instead as a shift in the radius of curvature of the optic, δR , as

$$\frac{1}{\delta R} = \frac{\alpha}{2\pi\omega^2\kappa} P_a, \quad (14)$$

where ω is the beam size. This relationship is specific to the case of an optic which is heated at the surface by a beam being reflected from it, but a similar relationship exists for optics heated in the bulk[16].

Since the dominant change in resonant optical cavities heated by optical absorption is a shift in the radii of curvature of the mirrors, a measurement of the frequency of any one of the HOM resonances is sufficient to characterize the thermal state of the cavity. In the following sections we exploit this fact in two particular ways; we use it to measure the absorption of the aLIGO IMC, and we use it to generate an error signal for the thermal state of the aLIGO PRC.

5 Input Mode Cleaner

The thermal characterization technique was first applied to the input mode cleaner (IMC) at the LIGO Livingston Observatory. The IMC is an in-vacuum, suspended, triangular optical cavity whose role in the aLIGO detectors is, amongst others, to suppress higher-order spatial modes on the input beam before injection into the main interferometer. Figure 1 shows the experimental layout. The IMC is formed by the three mirrors MC1, MC2, and MC3, and is outfitted with a resonant RF photodiode (RFPD) for length sensing and two differential wavefront sensors, WFSA and WFSB, for alignment sensing [17]. An active control system uses these signals to maintain the IMC on resonance for the fundamental mode of the carrier beam as well as to keep it aligned to this mode. The length control loops have a unity gain frequency (UGF) of 70 kHz while the angular loops have a UGF of 500 mHz.

While the cavity is maintained on resonance by the control system, a network analyzer and RF amplifier are used to add a pair of RF sidebands to the carrier beam by phase modulation applied with an electro-optic modulator (EOM). Downstream of the EOM the beam is partially occulted by placing a small metal pin into the beam, generating HOMs on both the sideband and the carrier out of the initially mostly HG₀₀ beam. A sample of the light in transmission of the IMC is picked off and brought out of the vacuum system where it is occulted in a similar manner and focused onto a broadband RFPD. The signal from this RFPD is fed to the network analyzer where it is demodulated at the RF modulation frequency.

Figure 2 shows data taken with this measurement across a full FSR of the IMC. The data are shown together with a FINESSE [18] model of the measurement and labels for the particular spatial mode order of each of the peaks. This figure shows that modes up to order four are visible with this measurement without using a more complicated strategy for HOM creation and detection. This experiment was used to track the HG₁₀ resonance of the IMC while the input power was cycled. The shift in this peak was used to infer the absorption in the IMC.

Although the Winkler approximation, discussed in Section 4, is useful for illustrating the physics behind the shift in first-order mode resonance and thus the measurement principle, in practice the situation is more complicated. The thermal distortion produced by absorption of the beam on the coating is not a strictly parabolic deformation. The effective curvature seen by each higher-order mode is different due to their different intensity profiles. As a general rule of thumb; the higher the mode order, the less effective curvature change it experiences for a thermal distortion produced by absorption of the fundamental mode. A numerical model was therefore used to convert shifts in the HG₁₀ resonance into absorption at the optic surfaces in order to take such effects into account.

The numerical model begins by calculating the deformation of the surface of the mirrors using a finite element model in the commercial software package COMSOL. The surface deformation is calculated for various levels of absorbed power ranging from 1 mW to 20 mW.

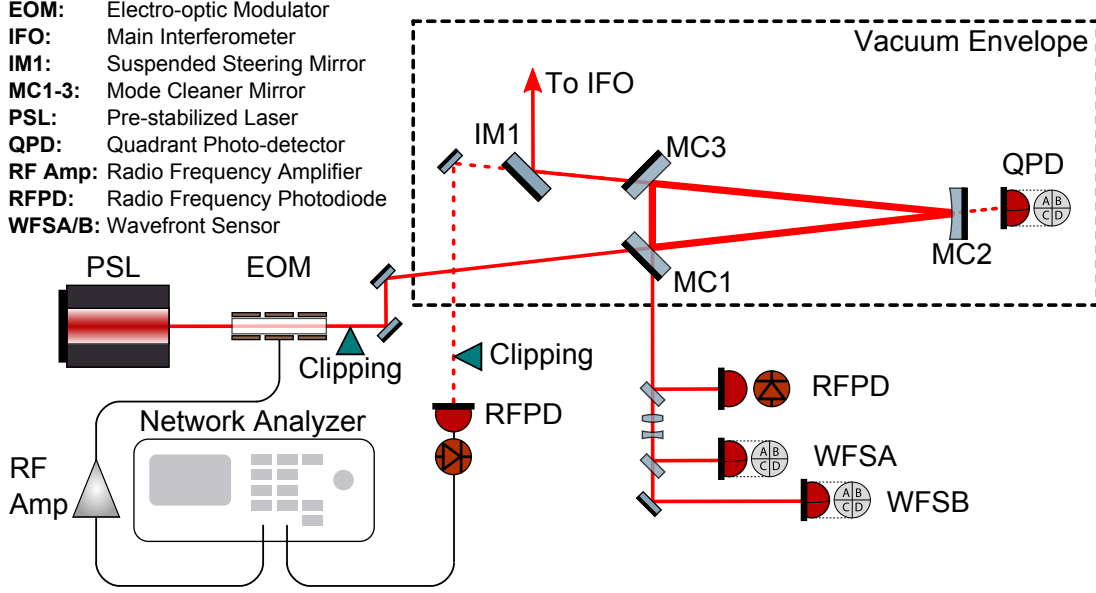


Figure 1: The experimental setup of the IMC eigenspectrum measurement. The probe beam is generated by adding phase sidebands to the resonant carrier beam with the aLIGO electro-optic modulator, and the signal is generated by demodulating in transmission.

These deformation maps are used together with the measured phase maps of the optics in an fast Fourier transform (FFT) based simulation which uses FFT beam propagation to calculate the stable mode in an optical cavity. Once the stable mode is calculated, the location of the first order resonance is identified by numerically adding RF sidebands to the beam similar to the real experiment. The numerical model assumes that the absorption is the same at all three mirrors.

Table 1 shows the results of this measurement during various repetitions taken over the course of nearly a year and a half. The final column shows the absorption inferred from the numerical model which assumes that the absorption is the same at each mirror. Throughout the time period over which these measurements were made, the vacuum chambers in which the IMC optics are suspended were variously vented, and the optics cleaned before re-evacuating the chambers. The apparent changes in absorption over time may therefore be attributable to the different states of the optics at the time of each measurement.

6 Power Recycling Cavity

A similar technique was applied to the power recycling cavity (PRC) of the aLIGO interferometers in order to sense their thermal state. The power recycling technique, employed in both initial LIGO and aLIGO, redirects light reflected from the Michelson interferometer back into the interferometer with the advantageous effects of increasing the circulating power and filtering the noise of the input beam while maintaining the bandwidth of the instrument's response to gravitational wave signals [1]. The increase in power reduces the shot noise equivalent strain, thus increasing the detector's sensitivity.

This increase in circulating power is not, however, without cost. Small yet finite absorption in the test masses of the interferometer coupled with non-zero thermo-elastic and thermo-optic coefficients cause deleterious thermal effects when operating the interferometer at high power. Both the input test masses (ITMs) and end test masses (ETMs) suffer from a shift in their radii of curvature as was described in Section 4. In addition, the non-zero thermo-optic coefficient leads to a significant thermal lens in the test

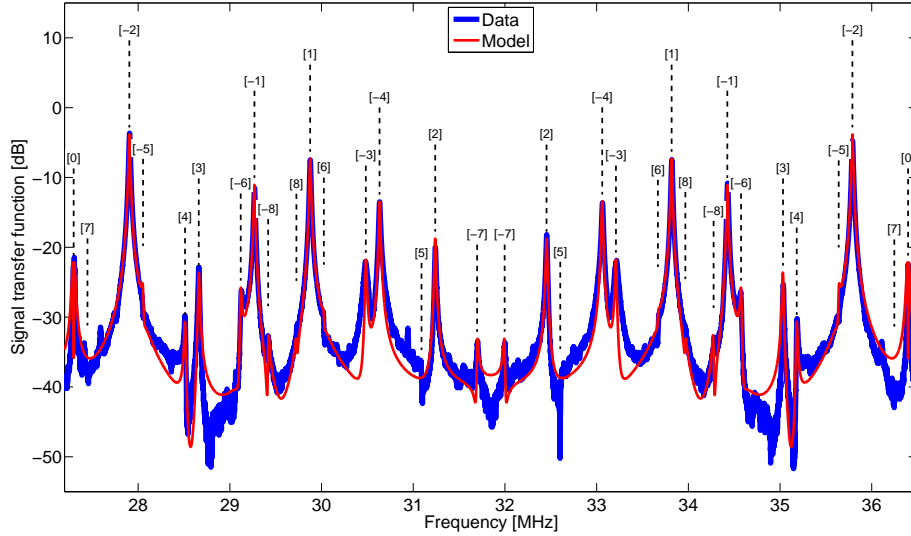


Figure 2: The magnitude of an example sweep across a full free spectral range of the input mode cleaner (IMC) together with a FINESSE model. The peaks are labeled with their spatial mode orders ($n + m$) with a minus sign indicating the split peaks of the odd orders (n). Since the IMC eigenspectra is probed with phase modulation, each peak appears twice from being excited independently by the upper and lower sideband.

mass substrates. The substrate thermal lens in the ITMs plays a role in determining the geometry of the PRC because the ITM substrates are situated within the PRC formed between the power recycling mirror (PRM) and reflective surfaces of both ITMs (see Figure 3). Both the thermo-optic and thermo-elastic effects act, to first order, to change the effective radii of curvature of the mirrors as sensed by the light circulating in the PRC. Hence, tracking of the first order resonance provides an excellent method of monitoring these thermal effects.

Figure 3 shows the layout of the experiment used to track the first order resonance of the PRC. It was necessary to inject an auxiliary laser into the interferometer after the IMC, because the IMC strips off any sidebands added to the input beam that are not integer multiples of its FSR. This auxiliary laser is phase locked to the main interferometer beam with an offset which is set by the RF output of a voltage controlled oscillator (VCO) with a center frequency at 27.3 MHz, a multiple of the cavity FSR. The phase locking is accomplished by combining a pickoff of the main beam and the auxiliary beam on an RFPD. The beatnote from this RFPD is high-pass filtered and mixed with the RF output of the VCO using a Minicircuits ZRPD-1 phase detector. The low-pass filtered output from this phase detector is fed through a simple servo to the frequency actuator in the auxiliary laser, thereby closing a phase-locked loop with a UGF of 50 kHz.

The auxiliary laser beam is occulted before being injected into the interferometer to generate HOMs, and the reflected beam from the interferometer, including both the carrier and sideband, is picked off by the in-vacuum Faraday isolator and a sample of the light is brought to an out-of-vacuum optical table. This sample of the reflected beam is occulted in a similar manner to the input beam before being focused onto a broadband RFPD. The signal from the RFPD is demodulated against the VCO signal which is slightly delayed in order to ensure that the output of the mixer is in the optimal quadrature for sensing the beat signal between the fundamental and first order modes. This signal is fed through a simple f^{-1} servo whose output drives the VCO, closing a feedback loop with a UGF of 1 Hz. The output of the servo is proportional to the frequency output of the VCO and is recorded into the aLIGO digital controls system.

Date	Power (W)	f_{10} (Hz)	Δf_{10} (Hz)	Abs. (ppm/mir.)
1/17/2013	3.11	$29,266,891 \pm 60$	$6,230 \pm 69$	2.39 ± 0.02
	30.5	$29,273,121 \pm 35$		
7/23/2013	0.517	$29,268,352 \pm 65$	245 ± 85	1.50 ± 0.46
	1.03	$29,268,597 \pm 56$		
8/6/2013	0.203	$29,267,831 \pm 14$	358 ± 15	1.42 ± 0.06
	1.01	$29,268,189 \pm 6$		
9/30/2013	1.07	$29,266,056 \pm 39$	$1,175 \pm 54$	1.53 ± 0.06
	3.08	$29,267,230 \pm 37$		
6/17/2014	1.79	$29,269,212 \pm 23$	$1,585 \pm 42$	0.50 ± 0.01
	10.2	$29,270,797 \pm 36$		

Table 1: The data and inferred absorption from numerous repetitions of the Gouy phase absorption measurements in the LLO IMC. The Power and f_{10} columns show the input power level and location of the TEM₁₀ peak while the δf_{10} and Abs. columns show the shift in this peak between power levels and the inferred absorption.

The result of this experimental setup is that the frequency of the auxiliary laser is locked to the first order resonance of the aLIGO PRC. The frequency of this resonance relative to the fundamental resonance is a tracer for the thermal state of the interferometer, and can be used as a feedback signal to the aLIGO thermal compensation systems (TCS) to maintain the interferometer in a particular thermal state. Using the Winkler approximation described in Section 4 together with the ray matrix techniques described in Section 3 and assuming that the effective radius of curvature of the two ITMs shift in unison, we can derive the round-trip Gouy phase change of the first order mode to be

$$\Delta\Psi_{00} = 0.701 \text{ rad} + 0.014 \frac{\text{rad}}{\mu\text{D}} \delta p, \quad (15)$$

where $\delta p = \frac{1}{\delta R}$ is the change in the mirror curvature. This can be converted to the frequency shift of the first order mode using Eqn. (11) where the round-trip length of the PRC is $L = 115.232 \text{ m}$.

Figure 4 shows the result of an experiment in which optical absorption in the PRC is simulated by applying equal amounts of heat to the two transmissive compensation plates which are situated directly in front of the input test masses with two CO₂ lasers operating at a wavelength of $10.6 \mu\text{m}$. At this wavelength nearly all of the optical power applied by the lasers is absorbed at the compensation plates. The size of the beam projected onto the compensation plates is roughly matched to the size of the science beam and thus provides an excellent stand-in for optical absorption. The compensation plates are located extremely close to the ITMs relative to the beam Rayleigh range and thus lensing in these plates causes an almost identical change in the PRC eigenmode to lensing in the ITMs themselves. Henceforth we therefore refer to lensing produced in the compensation plates simply as lensing in the ITM.

During the experiment, the change in the radius of curvature (ROC) of the ITMs as measured by the Advanced LIGO Hartmann wavefront sensors [19] (HWS) was also recorded. These devices use an aperture array in front of a CCD to image the wavefront of a beam reflected from each ITM. The optical setup of the HWS is designed such that the imaged wavefront is in an image plane of the ITM so that a change in the effective ROC of the ITM shows up as a change in the wavefront curvature at the HWS.

Equation 15 was used to convert the frequency shift of the first order resonance into the ROC shift of the ITMs. Figure 4 shows that the ROC shift measured by the first order resonance and that measured by the HWS are in good agreement. The residual disagreement is likely attributable to errors in the HWS calibration. This highlights an advantage of the first order resonance tracking over that of the HWS. Tracking of the first order resonance measures precisely the effective radius of curvature which is seen by the main resonant beam. The significantly better SNR of the first order resonance over that of the HWS

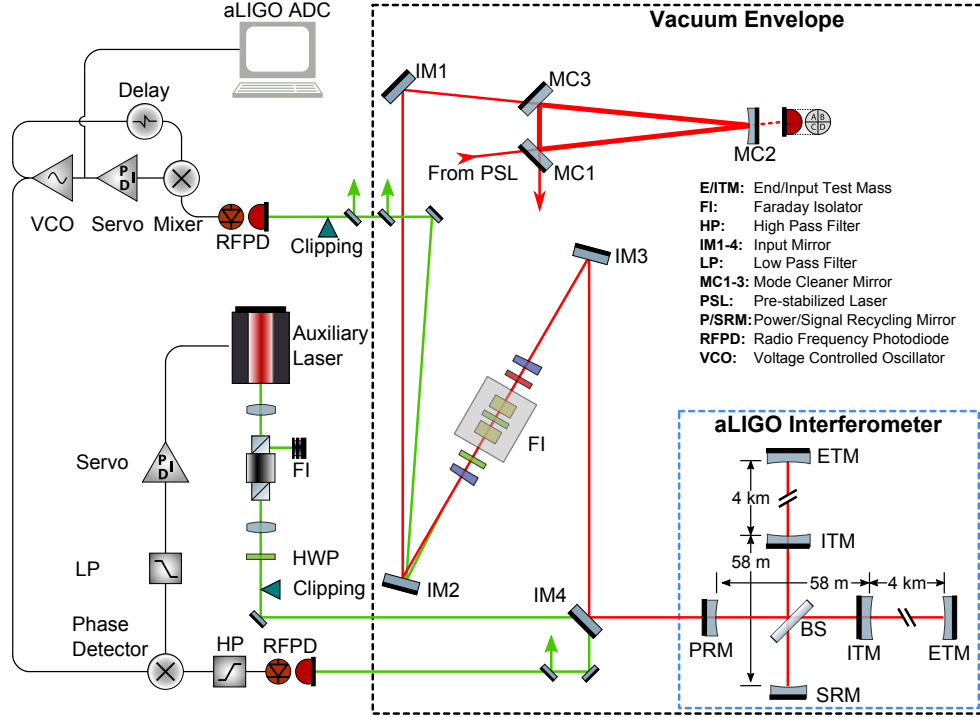


Figure 3: The experimental setup of the PRC thermal state sensor.

showcases another of its advantages. One disadvantage however is that the first order mode tracking method requires the PRC to be locked, whereas the HWS can operate independent of the resonance condition of the interferometer.

7 Conclusion and Outlook

In conclusion, tracking of the $HG_{10/01}$ mode resonance was shown to provide an excellent tracer for the thermal state of an optical resonator. This method was applied to measure the optical absorption of the input mode cleaner (IMC) at the LIGO Livingston Observatory. Although ultra-low absorption in the IMC is not essential to the overall operation of gravitational wave interferometers, monitoring the absorption over time provides an excellent method of tracking the degradation, or lack thereof, of the optical coatings over the long time periods for which these devices are designed to operate. It can also be used as a method of validating the cleanliness of the vacuum system after incursions for repairs or maintenance.

It was also shown that real-time tracking of the thermal state of the resonant cavities of interferometric gravitational wave detectors is possible by tracking the first-order resonance. This represents a significant breakthrough in thermal state sensing since all previous monitors have only been able to monitor the thermal state of individual mirrors. In contrast, tracking of the first excited mode provides a thermal error signal which is directly tied to the configuration of the interferometer.

The technique applied to track the thermal state of the Advanced LIGO power recycling cavity (PRC) could be extended to sense the thermal state of the other resonant cavities in interferometric gravitational wave detectors. Doing so would provide independent thermal error signals for all of the important thermal degrees of freedom of these devices, thus making the process of compensating for thermal distortions more deterministic and repeatable than in previous states of operation.

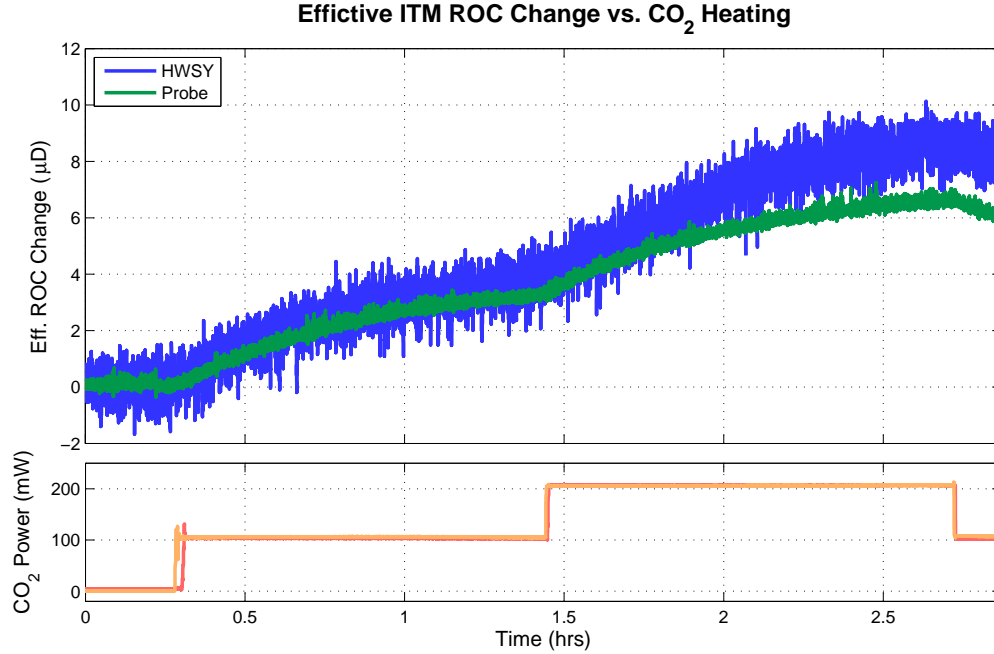


Figure 4: The shift in the resonant frequency of the first order excited mode is shown while the cavity is heated with CO₂ lasers projected onto the test masses. The shift in the resonant frequency is converted into a shift of the radius of curvature of the test mass through a ray matrix model described in the text. Also shown is the effective ROC shift in the test masses as measured by a Hartmann wavefront sensor.

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